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**APPLICATION FOR UNITED STATES LETTERS PATENT**

**FOR**

**APPARATUS AND METHOD FOR RESISTIVITY MEASUREMENTS DURING  
ROTATIONAL DRILLING**

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## **CROSS REFERENCES TO RELATED APPLICATIONS**

This application is a continuation-in-part of United States Patent Application Ser. No. 09/836,980 filed on 18 April 2001.

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## **BACKGROUND OF THE INVENTION**

### **1. Field of the Invention**

[0001] The present invention relates to well logging. In particular, the present invention is an apparatus and method for imaging of subsurface formations using electrical  
10 methods.

### **2. Background of the Art**

[0004] *Birdwell* (US Patent 3,365,658) teaches the use of a focused electrode for determination of the resistivity of subsurface formations. A survey current is emitted  
15 from a central survey electrode into adjacent earth formations. This survey current is focused into a relatively narrow beam of current outwardly from the borehole by use of a focusing current emitted from nearby focusing electrodes located adjacent the survey electrode and on either side thereof. *Ajam et al* (US Patent 4,122,387) discloses an apparatus wherein simultaneous logs may be made at different lateral distances through a  
20 formation from a borehole by guard electrode systems located on a sonde which is lowered into the borehole by a logging cable. A single oscillator controls the frequency of two formation currents flowing through the formation at the desired different lateral

depths from the borehole. The armor of the logging cable acts as the current return for one of the guard electrode systems, and a cable electrode in a cable electrode assembly immediately above the logging sonde acts as the current return for the second guard electrode system. Two embodiments are also disclosed for measuring reference voltages between electrodes in the cable electrode assembly and the guard electrode systems

[0005] Techniques for investigating the earth formation with arrays of measuring electrodes have been proposed. See, for example, the U.S. Pat. No. 2,930,969 to *Baker*, Canadian Pat. No. 685,727 to *Mann et al.* U.S. Patent No. 4,468,623 to *Gianzero*, and U.S. Patent No. 5,502,686 to *Dory et al.* The *Baker* patent proposed a plurality of electrodes, each of which was formed of buttons which are electrically joined by flexible wires with buttons and wires embedded in the surface of a collapsible tube. The *Mann* patent proposes an array of small electrode buttons either mounted on a tool or a pad and each of which introduces in sequence a separately measurable survey current for an electrical investigation of the earth formation. The electrode buttons are placed in a horizontal plane with circumferential spacings between electrodes and a device for sequentially exciting and measuring a survey current from the electrodes is described.

[0006] The *Gianzero* patent discloses tool mounted pads, each with a plurality of small measure electrodes from which individually measurable survey currents are injected toward the wall of the borehole. The measure electrodes are arranged in an array in which the measure electrodes are so placed at intervals along at least a circumferential direction

(about the borehole axis) as to inject survey currents into the borehole wall segments which overlap with each other to a predetermined extent as the tool is moved along the borehole. The measure electrodes are made small to enable a detailed electrical investigation over a circumferentially contiguous segment of the borehole so as to obtain indications of the stratigraphy of the formation near the borehole wall as well as fractures and their orientations. In one technique, a spatially closed loop array of measure electrodes is provided around a central electrode with the array used to detect the spatial pattern of electrical energy injected by the central electrode. In another embodiment, a linear array of measure electrodes is provided to inject a flow of current into the formation over a circumferentially effectively contiguous segment of the borehole. Discrete portions of the flow of current are separably measurable so as to obtain a plurality of survey signals representative of the current density from the array and from which a detailed electrical picture of a circumferentially continuous segment of the borehole wall can be derived as the tool is moved along the borehole. In another form of an array of measure electrodes, they are arranged in a closed loop, such as a circle, to enable direct measurements of orientations of resistivity of anomalies

[0007] The *Dory* patent discloses the use of an acoustic sensor in combination with pad mounted electrodes, the use of the acoustic sensors making it possible to fill in the gaps in the image obtained by using pad mounted electrodes due to the fact that in large diameter boreholes, the pads will necessarily not provide a complete coverage of the borehole.

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[0009] Co-pending United States Patent Application Ser. No. 09/836,980 of *Evans et al* -----

("the *Evans* '980 application"), the contents of which are fully incorporated herein by reference, discloses a device suitable for resistivity imaging with water based mud (WBM) and oil based mud (OBM). The device disclosed in the *Evans* '980 application is basically a wireline logging device. United States Patent 6600321 to *Evans* discloses a modification of the *Evans* '374 application that is adapted for use in measurement while drilling (MWD) applications. Both of the *Evans*' applications have pad mounted electrodes that are in contact with the earth formation.

10 [0010] Another device that could be used for MWD resistivity measurements is the one described in US Patent 6,173,793 to *Thompson et al*. In *Thompson*, the drill bit may be driven by a downhole drilling motor. The motor may be on a rotating drillstring or on coiled tubing. The sensors for measuring the parameters of interest could be rotating with the drill bit. Alternatively, the sensors could have one of several configurations. In  
15 one configuration, the sensors are mounted on a substantially non-rotating sleeve; in another configuration, the sensors are mounted on pads that could be rotating or non-rotating, the pads being hydraulically or mechanically actuated to make contact with the borehole wall; in yet another configuration, the sensors are mounted on substantially non-rotating rib-steering devices used to control the direction of the downhole drilling tool.  
20 In any of these arrangements, the downhole assembly is provided with sensors that make measurements of the parameters of interest. The assembly is provided with magnetic and inertial sensors to provide information on the orientation of the measurement sensors. A

telemetry system sends information downhole about the depth of the drilling assembly. A microprocessor downhole combines the depth and azimuth information with the measurements made by the rotating sensors, uses redundancy in the data to improve S/N ratio, compresses the data and sends it uphole by a telemetry system. ..

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[0011] The devices of *Evans* and of *Thompson* when used for resistivity imaging suffer from one significant drawback. Being contact devices, there is considerable wear on the sensors. The *Evans* devices comprise a plurality of sensing electrodes and are relatively bulky. The *Thompson* device is best suited for use with a slowly rotating sleeve. With a slowly rotating sleeve, it may not be possible to get a full 360<sup>0</sup> image of the borehole.

[0012] It would be desirable to have a resistivity imaging apparatus and method for providing MWD images of earth formations. Such a device should preferably be operable with OBM and WBM. It is also preferable that the device should be relatively simple and not be subject to undue wear and tear in MWD operations. The present invention satisfies this need.

### **SUMMARY OF THE INVENTION**

[0013] The present invention is an apparatus and method of obtaining a resistivity image of a borehole during drilling operations. A resistivity sensor is maintained at a specified standoff from the borehole wall using a suitable device. A processor uses measurements

from an orientation sensor on the resistivity sub for determining a toolface orientation during continued rotation. The resistivity sensor may be mounted on a pad, rib, or a stabilizer. The resistivity sensor may be galvanic and may include suitable focusing, guard and monitor electrodes. A variety of focusing techniques may be used. A processor, preferably downhole, may be used for maintaining a substantially constant power consumption. The orientation sensors may be a magnetometer, an accelerometer, or a gyroscope. In oil based mud, capacitive coupling may be used. Multifrequency measurements may be used in combination with known frequency focusing techniques.

10 [0014] Non-galvanic sensors may also be used for making resistivity measurements. These include induction sensors, and may further include a shielded dipole or a quadrupole antenna for directionality. A ground penetrating radar may be used for monitoring fluid invasion into the earth formation.

15 **BRIEF DESCRIPTION OF THE FIGURES**

[0015] The file of this patent contains at least one drawing executed in color: Copies of this patent with color drawing(s) will be provided by the Patent and Trademark Office upon request and payment of the necessary fee.

20 [0016] The novel features that are believed to be characteristic of the invention, both as to organization and methods of operation, together with the objects and advantages thereof, will be better understood from the following detailed description and the drawings

wherein the invention is illustrated by way of example for the purpose of illustration and description only and are not intended as a definition of the limits of the invention:

**Fig. 1** (prior art) is a schematic illustration of a drilling system

- 5    **Fig. 2** is an exemplary configuration of the various components of a resistivity measuring sensor sub

**Figs. 3a - 3d** show exemplary configurations of a resistivity measuring sub.

**Fig. 4** shows an exemplary illustration of a galvanic sensor

**Fig. 5** shows another exemplary illustration of a galvanic sensor.

- 10   **Fig. 6** is an exemplary block diagram of an arrangement for maintaining constant power consumption.

**Fig. 7.** (prior art) shows an electrode configuration according to one embodiment of the present invention.

**Fig. 8.** is a block diagram of an arrangement for compensating for contact resistance.

- 15   **Fig. 9** is an illustration of a model showing a resistivity measuring device according to the present invention in proximity to a bed boundary.

**Fig. 10** shows simulated azimuthal responses for the configuration of **Fig. 9** for various distances of the tool from the bed boundary

- 20   **Fig. 11** shows model measurements using the device of the present invention in proximity to a model.

**Fig. 12a** shows a physical model for testing the apparatus of the present invention.

**Fig. 12b** (in color) shows an exemplary image obtained using the apparatus of the



present invention in a model.

**Fig. 13** shows an example of a shielded magnetic dipole suitable for use in an embodiment of the present invention.

**Fig. 14.** shows an example of a quadrupole induction system suitable for use in an  
5 embodiment of the present invention.

**Fig. 15** (prior art) shows an example of ground penetrating radar measurements used for monitoring a fluid interface in a model study.

**Fig. 16** (prior art) shows use of an induction coil as a resistivity sensor.

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## **DETAILED DESCRIPTION OF THE INVENTION**

[0017] **FIG. 1** shows a schematic diagram of a drilling system **10** with a drillstring **20** carrying a drilling assembly **90** (also referred to as the bottom hole assembly, or "BHA") conveyed in a "wellbore" or "borehole" **26** for drilling the wellbore. The drilling system **10** includes a conventional derrick **11** erected on a floor **12** which supports a rotary table  
15 **14** that is rotated by a prime mover such as an electric motor (not shown) at a desired rotational speed. The drillstring **20** includes a tubing such as a drill pipe **22** or a coiled-tubing extending downward from the surface into the borehole **26**. The drillstring **20** is pushed into the wellbore **26** when a drill pipe **22** is used as the tubing. For coiled-tubing applications, a tubing injector, such as an injector (not shown), however, is used to move  
20 the tubing from a source thereof, such as a reel (not shown), to the wellbore **26**. The drill bit **50** attached to the end of the drillstring breaks up the geological formations when it is rotated to drill the borehole **26**. If a drill pipe **22** is used, the drillstring **20** is coupled

to a drawworks **30** via a Kelly joint **21**, swivel, **28** and line **29** through a pulley **23**.

During drilling operations, the drawworks **30** is operated to control the weight on bit, which is an important parameter that affects the rate of penetration. The operation of the drawworks is well known in the art and is thus not described in detail herein.

5

[0018] During drilling operations, a suitable drilling fluid **31** from a mud pit (source) **32** is circulated under pressure through a channel in the drillstring **20** by a mud pump **34**.

The drilling fluid passes from the mud pump **34** into the drillstring **20** via a desurger **36**, fluid line **28** and Kelly joint **21**. The drilling fluid **31** is discharged at the borehole

10 bottom **51** through an opening in the drill bit **50**. The drilling fluid **31** circulates uphole through the annular space **27** between the drillstring **20** and the borehole **26** and returns to the mud pit **32** via a return line **35**. The drilling fluid acts to lubricate the drill bit **50** and to carry borehole cutting or chips away from the drill bit **50**. A sensor **S<sub>1</sub>** preferably placed in the line **38** provides information about the fluid flow rate. A surface torque  
15 sensor **S<sub>2</sub>** and a sensor **S<sub>3</sub>** associated with the drillstring **20** respectively provide information about the torque and rotational speed of the drillstring. Additionally, a sensor (not shown) associated with line **29** is used to provide the hook load of the drillstring **20**.

20 [0019] In one embodiment of the invention, the drill bit **50** is rotated by only rotating the drill pipe **22**. In another embodiment of the invention, a downhole motor **55** (mud motor) is disposed in the drilling assembly **90** to rotate the drill bit **50** and the drill pipe **22** is

rotated usually to supplement the rotational power, if required, and to effect changes in the drilling direction.

[0020] In the preferred embodiment of **Fig. 1**, the mud motor **55** is coupled to the drill bit **50** via a drive shaft (not shown) disposed in a bearing assembly **57**. The mud motor rotates the drill bit **50** when the drilling fluid **31** passes through the mud motor **55** under pressure. The bearing assembly **57** supports the radial and axial forces of the drill bit. A stabilizer **58** coupled to the bearing assembly **57** acts as a centralizer for the lowermost portion of the mud motor assembly.

10

[0021] Turning now to **Fig. 2**, an exemplary configuration of the various components of the resistivity measuring sensor sub are shown. At the upper end, a modular cross-over sub **101** is provided. The power and processing electronics are indicated by **103**. The sub is provided with a stabilizer **107** and a data dump port may be provided at **105**. A resistivity sensor (discussed further below) are provided at **109** with the sensor and measuring electronics at **113**. Modular connections **115** are provided at both ends of the sub that enable the sub to be part of the bottom hole drilling assembly. An orientation sensor **111** is provided for measuring the toolface angle of the sensor assembly during continued rotation. Different types of orientation sensors may be used, including magnetometers, accelerometers, or gyroscopes. Use of such devices for determination of the toolface angle are known in the art and are not discussed further herein.

20

[0022] The stabilizer shown at **107** serves several important functions. Like conventional stabilizers, one function is to reduce oscillations and vibrations of the sensor assembly. However, in the context of the present invention, it also serves another important function, viz, centralizing the portion of the bottom hole assembly (BHA) including a sensor assembly, and also maintaining the sensors with a specified standoff from the borehole wall. This is not visible in **Fig. 2**, but the outer diameter of the stabilizer is greater than the outer diameter of the portion of the BHA including the resistivity sensor. As a result of this difference in diameter, the resistivity sensor is maintained with a standoff from the borehole wall during continued rotation of the drillstring, hence avoiding the problems with wear associated with the prior art devices such as *Thompson*, and *Evans*.

[0023] Turning now to **Fig. 3a**, an exemplary configuration of the various components is shown. A stabilizer is shown at **125**, the resistivity sensor is generally depicted at **121** and the associated electronics are shown generally at **122**. As shown in **Fig. 3a**, the resistivity sensor could be any one of the types described further below. The orientation sensor is depicted at **123**. In **Fig. 3b**, the arrangement is similar to that of **Fig. 3a** with the difference that the resistivity sensor **123'** may be deployed on the stabilizer. The configuration in **Fig. 3c** depicts an additional portion of the resistivity sensor by **124''**. This is meant to generally depict a somewhat more complicated resistivity sensor: for example, as shown in **Fig. 3c**, the portion **121** could be a current electrode and the portion **124''** could depict electronics associated with a guard electrode. **Fig. 3d** shows

another possible arrangement of the components shown in **Fig. 3c**. The point to be made here is that a wide variety of types of resistivity sensors may be used, and the disposition of the resistivity sensors, associated electronics, and orientation sensors could be quite varied. When the resistivity sensor is deployed on a stabilizer, it is recessed so as to avoid contact between the sensor and the borehole wall.

[0024] There are a number of different configurations by which the sensor assembly may be coupled to the drill collar. In one embodiment of the invention, the sensor is installed at a fixed position on the drill-collar, so that it rotate with exactly the same rotational speed as the drillstring does. One possible drawback of such an arrangement is the vast amount of data that would result. The rate of penetration of a bottom hole assembly is relatively slow, so that with a typical rotational speed of 60 rpm, the data that are acquired have a high amount of redundancy. In some situations where the signal to noise ratio (SNR) is low, the redundancy can be advantageous and the data can be stacked to improve the SNR. However, in many instances, this may not be necessary. At the other extreme is the arrangement described in *Thompson et al.* where the sensors are mounted on a substantially non-rotating sleeve. The possible drawback of such an arrangement is that if the rotation rate of the sleeve is too slow, the borehole wall may be inadequately sampled by a single resistivity sensor. As taught in *Thomson et al.*, a plurality of sensors, possibly on a plurality of pads, may be used: this leads to a more complicated system. Accordingly, in a preferred embodiment of the present invention, the sensor is mounted on a sleeve which rotates by a separate drive. In this case, the movement of the

electrodes is uncoupled from the rotation of the drillstring. This makes it possible to

control the azimuthal sampling of the borehole wall as well as the amount of redundancy in the data. In any case, the distance of the electrode surface to the formation is maintained by a near by stabilizer. In an optional embodiment of the invention, steerable  
5 ribs which are used to keep the exact distance. The separate drive may include a stabilizer. In addition and for further failure correction, the stand off will be monitored by means of acoustic calipers.

[0025] Turning now to **Fig. 4**, one configuration of the resistivity sensor is shown. This

10 particular resistivity sensor is a galvanic sensor that operates by conveying a measure current into the formation. The measure electrode is indicated by **151**, the guard electrode is denoted by **153**, an insulating section by **155** and the return path for the electrical current from the measure electrode is through the body shown by **157**. In an alternate embodiment of the invention, shown in **Fig. 5**, the measure electrode is denoted  
15 by **201**, a first guard electrode by **203**, an insulating section by **205**, a second guard electrode by **209**, a second insulating section by **211**. For shallow depth of investigation, **203** can be the guard and **209** is the return electrode. For deeper investigation, **203** and **209** are maintained at the same potential and the return path for the electrical current is through the body **213**. Those versed in the art would recognize that with the  
20 configurations shown in **Figs. 3 and 4**, any of the commonly used galvanic sensory arrangements can be implemented, as discussed below.

~~[0026]~~ One possible arrangement is of the commonly used device known as the laterolog  
Current is sent between different guard electrodes to achieve different depths of  
investigation into the formation.. In the configuration referred to as a microlaterolog,  
guard electrode surrounds said measure electrode and maintains a focusing of said  
5 measure current in a flushed zone of said formation. The electrodes may be configured to  
create substantially spherical equipotential surfaces. This is referred to as spherical  
focusing. In the "short normal" configuration, a current electrode conveys a measure  
current into said formation, and voltage is measured at a measure electrode spaced apart  
from said current electrode From the voltage of the measure electrode and the measure  
10 current, an indication of a resistivity of said earth formation is obtained. In a particular  
embodiment of the present invention, the guard electrode may extend the full  
circumference of the tool. All of these are known in the art and are not discussed further.

[0027] The present invention provides a control of the voltage and/or the current at guard  
15 and measurement electrodes.. There are several methods of doing this. For achieving an  
optimal focusing guard and measurement electrode need to be kept on almost the same  
potential. An improvement of the SNR for the measurement in very high resistive  
formations could be provided by increasing the voltage on the measurement electrode.  
Due to the coupling of potential between measurement and guard electrode the guard  
20 current would increase dramatically by keeping such a high voltage in low resistive  
formations. To overcome this problem voltage and/or current of the guard and/or  
measurement electrode can be controlled, for instance by keeping the power constant.

----- This is shown in **Fig. 6**. The power supply **301** is controlled by the controller **303** in  
response to a signal  $\Delta U$  **323**. This signal  $\Delta U$  is obtained as a ratio of a power difference  
 $\Delta \text{Sqrt}P$  **307** and an apparent resistance  $R_{app}$ . The power difference  $\Delta \text{Sqrt}P$  is obtained  
as a difference between square roots of a nominal power  $P_{nom}$  **311** and an actual power  
5 consumed  $P_{act}$  **321**., the difference being determined at **309**. The apparent resistance  $R_{app}$   
is obtained from the product **317** of the electrode potential  $U_{act}$  **315** and the reciprocal of  
the measure current  $I_{act}$ . (The product **319** of  $U_{act}$  **315** and the measure current  $I_{act}$  gives  
the actual power  $P_{act}$  **321**). If the tool enters a formation with a different resistivity **313**,  
the current through the formation and therefore the electrical power will change. The  
10 voltage will be controlled so that the electrical power will stay constant. Other controlling  
methods, for instance controlling by keeping current or voltage constant, are also  
possible.

[0028] One of the potential problems that have to be considered is the effect of contact  
15 impedances. Compensating for these effects is discussed next with reference to **Figs. 7**  
and **8**. Shown in **Fig. 7** is a focused arrangement with the current electrode denoted by  
**405** and the guard electrode denoted by **401**. In the example, two concentric monitor  
electrodes are shown by **403** and **407**. The right hand portion of **Fig. 7** shows current  
flows into the formation. If **401** and **405** have the same electrical potential, then  
20 existence of a voltage difference between the monitor electrodes **403** and **407** is an  
indication of significant contact impedance. **Figure 8** illustrates a controlling diagram  
for keeping the monitoring voltage **501** at a minimum (zero) **502** by varying for instance



the voltage on the measurement electrode **503**. The voltage on the guard electrode **504**

could be already adjusted for instance by means of a power control and assumed as

constant. The controller **505** will amplify (attenuate) and/or phase shift the signal of the guard electrode in order to generate the voltage on the measurement electrode **503**,

- 5 depending on the difference between monitoring electrode voltage **501** and minimum monitoring voltage **502**. This technique has been used for a longer time now in wireline applications (Serra, 1984).

[0029] The ability of a simple electrode system of **Fig. 4** to measure azimuthal variations  
10 of resistivity is illustrated next in **Figs. 9** and **10**. Shown in **Fig. 9** is a cross section of the tool in proximity to a bed boundary. The outer diameter of the drill pipe **607** is defined as “**D**”. The measure electrode is shown as **611** and the guard electrode by **609**. The resistivity of the upper layer **603** is  $1\ \Omega\ \text{m}$  while the resistivity of the lower layer **605** is  $100\ \Omega\ \text{m}$ .  $0^\circ$  azimuth (or toolface angle) is defined to be the tool orientation for which  
15 the measure electrode is away from the boundary while  $180^\circ$  azimuth is for the measure electrode towards the boundary. **Fig. 10** shows the variation of the measured resistivity (ordinate) as a function of azimuth (abscissa). The curve **701** corresponds to the case where the distance from the center of the drillpipe to the boundary is  $2D$ . Curves **703**,  
**705**, **707**, **709** and **711** show azimuthal variations for distances of  $1.5D$ ,  $1D$ ,  $0.75D$ ,  $0.5D$   
20 and  $0D$  respectively. Based on **Fig. 10**, it is thus possible to get an indication of close proximity to a bed boundary from azimuthal variations of apparent resistivity as measured by a galvanic resistivity sensor.

[0030] Another indication of the resolution of such a tool can be obtained from Fig. 11. The ordinate is the depth of the tool from the bed boundary. The abscissa is the current in the current electrode. The curve 751 shows the variation of the current for an azimuth of 0°. The current has a low value of approximately 0.2mA when the tool is below the boundary in the high resistivity medium (10 Ωm). This low current persists as the tool is moved up until, when the tool is 50 mm above the bed boundary, the current increases to about 0.8 mA in the low resistivity medium (1 Ωm). For a sensor at 180° azimuth (given by 769), the current starts changing value from the low to high when the center of the tool is 50 mm below the bed boundary. The other curves 753, 755, 757, 759, 761, 763, 765, 767 correspond to azimuths of 20° to 160° in 20° increments.

[0031] The apparatus and methods described above are suitable for use with water based mud (WBM) where the fluid in the borehole is conductive. With relatively minor modifications, the apparatus and methods can also be used in oil based mud (OBM). As discussed in the *Evans* '980 application and in *Evans et al*, galvanic measurements of earth formations can be made through an OBM by using capacitive coupling. As noted above, one important in which the present invention differs from the teachings of the *Evans* '980 application or the *Evans et al* patent is that the present invention is not a contact device. However, the principles of capacitive coupling as taught in either of the *Evans* documents can be used in the present invention. By operating at a sufficiently high frequency, the source current can be capacitively coupled into the formation. This is

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true for all of the embodiments discussed above.

[0032] The apparatus of the present invention can also be used to operate at a plurality of frequencies, and measurements made at a plurality of frequencies can be used to  
5 determine formation resistivities. This is taught in US Patent Application Ser. No. 10/347,019 of *Tabarovsky* et al, having the same assignee as the present application and the contents of which are fully incorporated herein by reference. The frequency is selected to make an impedance caused by the dielectric constant of the non-conducting fluid to be substantially less than a resistivity of said nonconductive fluid. In one  
10 embodiment of *Tabarovsky*, a dual frequency method is used for determining formation resistivity. In another embodiment taught by *Tabarovsky*, more than two frequencies are used and a multifrequency focusing method is used. Both of these methods may be used with the present invention.

15 [0033] The apparatus and method of the present invention may also be used by replacing the galvanic sensors with propagation resistivity sensors. These are designed to operate in the MHz to GHz frequency range. Typically, two transmitters are symmetrically disposed about two receivers, and by measuring the amplitude and/or phase of a received signal at the two receivers for a propagating signal in the earth formation, the formation  
20 resistivity may be determined. A particular example of such an arrangement is disclosed in a copending United States Patent Application of *Chemali* et al, having the title "Electrical Imaging in Conductive and Non-Conductive Mud" filed on July 8, 2003 under

incorporated herein by reference. The device taught therein can be operated at 10 MHz to 2 Ghz.

5 [0034] Turning now to **Fig. 12b**, an example of a resistivity image produced by a galvanic resistivity sensor according to the method of the present invention. For laboratory measurements a borehole simulation tool was built up where measurements can be simulated. The tank model used for the experiment is shown in **Fig. 12a**. The physical model **781** consists of two blocks of different materials (tuff **771** and sandstone  
10 **777** with a dipping boundary **775** between the two blocks. The tool (not shown) is conveyed into a cylindrical hole **773**. The annulus between the tool and the blocks **771** and **777** is filled with brine. The tool comprises a return, guard and measurement electrodes and the isolations between them. The stones are saturated with brine. From preliminary measurements resistivities of 66  $\Omega$ -m and 12 $\Omega$ -m are estimated for  
15 sandstone and tuff, respectively.

[0035] In another embodiment of the invention a shielded dipole antenna is used. This is schematically illustrated in **Fig. 13**. The dipole antenna, depicted here by a point dipole **803** is surrounded by a shield **801**. The axis of the dipole is directed radially away from  
20 the tool axis. Such a shielded antenna has stronger directional characteristics than an unshielded dipole antenna. Consequently, it is particularly suited for azimuthal imaging of borehole walls. The selection of angle  $\theta$  has to be a compromise between

directionality and the signal strength: the smaller the angle  $\theta$  the greater the directionality

(smaller aperture) but the less would be the signal strength. In a MWD device, the stacking over different rotations of the logging tool can be used to compensate for loss of the signal strength.

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[0036] In an alternate embodiment of the invention, a quadrupole antenna is used. This is schematically illustrated in **Fig. 14**. Shown by the arrows **851** are the preferred direction of a transmitter output while **853** depicts a radiation pattern. As can be seen, this has high directional sensitivity and can be used for azimuthal imaging. A particular feature of a quadrupole antenna is that when it is proximate to a bed boundary, it has directional sensitivity between up and down directions, whereas an unshielded dipole antenna may only be sensitive to presence of a bed boundary and cannot tell the difference between up and down directions, i.e., the position of the boundary relative to the tool.

15 [0037] In another embodiment of the invention, the resistivity sensor is a radar sensor of the type commonly referred to as ground penetrating radar (GPR). The operating frequency of such a radar may be in the range of 500 MHz to 10 GHz. This may be used to monitor the invasion of borehole mud, particularly OBM into earth formations. As discussed in *Peeters et al*, the reflection coefficient  $R$  at a plane interface between two media is given by

20

$$R = \frac{\mu_2 k_1 - \mu_1 k_2}{\mu_2 k_1 + \mu_1 k_2}$$

where the  $\mu$  's are the magnetic permeabilities of the two media and the  $k$  's are the wavenumbers. The wavenumber  $k$  is in turn related to the frequency  $\omega$  , the relative magnetic permeability  $\mu$ , the conductivity  $\sigma$  and the dielectric permittivity  $\epsilon$  by the following equation:

$$k^2 = \omega^2 \mu \epsilon - i \omega \mu \sigma$$

A significant contrast in at least one of  $\epsilon$  or  $\sigma$  will produce a noticeable radar reflection.

10 The contrast in  $\epsilon$  between oil and water is 81/5 for frequencies up to a few GHz.

Similarly, there is a significant contrast in  $\sigma$  between brine and fresh water.

[0038] **Fig. 15** shows prior art results from sandbox model studies using GPR. A GPR composite image is shown with visual observations of a fluid interface between two fluids superimposed. For the example shown, brine is invading a freshwater sandpack. The individual GPR images are processed images of data obtained using sources and receivers on the boundaries of the model. A conventional seismic migration algorithm was used for providing the images. The left side of the GPR image was acquired after 20 minutes and shows good agreement with the visual observations **871** after 10 minutes. 20 The right side of the GPR image was obtained after 45 minutes and shows good correspondence with the visual observations **875** that were made after 1 hour and 10

minutes. The top radar panel was acquired in between and the results fall between the two visual fronts. This model study shows that GPR can produce a reflection from an brine/freshwater interface. The present invention uses GPR measurements made using sources and receivers in the wellbore (in contrast to the prior art data of **Fig. 15** obtained using measurements on the boundaries of a sandbox model.) to monitor invasion of an OBM into a water saturated rock, or WBM into an oil bearing formation. Similarly, due to the contrast in  $\sigma$ , GPR can detect invasion of fresh water into a brine bearing rock.

[0039] Another embodiment of the invention uses an induction coil as a resistivity sensor.

10 In a conductive formation and OBM in the borehole, currents through the induction coil will induce eddy currents in the formation. By measuring changes in the resistance and inductive reactance of the coil, information can be gathered about the earth formation. This information includes the electrical conductivity and magnetic permeability of the material, the amount of material cutting through the coils magnetic field, and the  
15 condition of the material (i.e. whether it contains cracks or other defects.) The mutual inductance is affected by the standoff, and hence it is important to maintain the standoff at a selected value. This is illustrated in **Fig. 16**. Shown therein is a coil **905** in proximity to a conductive material such as an earth formation. The magnetic field lines from the coil are depicted by **903**. The induced eddy currents are shown by **901** and the  
20 magnetic field resulting from the eddy currents are shown by **907**. This basic principle has been used before for determining defects in casing.

[0040] The invention has been described above with reference to a device that is

conveyed on a drilling tubular into the borehole, and measurements are made during drilling. The processing of the data is preferably done downhole using a downhole processor at a suitable location. It is also possible to store at least a part of the data downhole in a suitable memory device, in a compressed form if necessary. Upon  
5 subsequent retrieval of the memory device during tripping of the drillstring, the data may then be retrieved from the memory device and processed uphole.

[0041] While the foregoing disclosure is directed to the preferred embodiments of the invention, various modifications will be apparent to those skilled in the art. It is intended  
10 that all variations within the scope and spirit of the appended claims be embraced by the foregoing disclosure.